

# Appendix I Survey Program Technical Memorandum

Wyckoff/Eagle Harbor Superfund Site

Bainbridge Island, WA September 25, 2017 This page is intentionally left blank.

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# Acronyms and Abbreviations

APS APS Mapping and Surveying

DEM Digital Elevation Model
EBS Exposure Barrier System

Ecology Washington State Department of Ecology

EHOU Eagle Harbor Operation Unit

EPA U.S. Environmental Protection Agency

FSP Field Sampling Plan

MBES multibeam echo sounder

MCA Miller Creek Aerial Mapping

MLLW mean lower low water

NOAA National Oceanic and Atmospheric Administration
OMMP Operations, Monitoring, and Maintenance Plan

QAPP Quality Assurance Project Plan

RGB Red/Green/Blue

SAIC Science Applications International Corporation

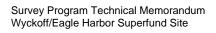
SBES single beam echo sounder

SEA Striplin Environmental Associates

SEE Science and Engineering for the Environment, LLC

USACE U.S. Army Corps of Engineers

USGS U.S. Geological Survey



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#### 1 Introduction

#### 1.1 Purpose

The purpose of this memorandum is to provide an assessment of the physical stability of the Exposure Barrier System (EBS) as outlined in the Year 22 – 2016 Operations, Monitoring, and Maintenance Plan (OMMP). This assessment is supported, in part, by the results of the recently-conducted survey program discussed in this memorandum.

This survey program technical memorandum is an appendix to the 2016 Year 22 Data Monitoring Report. The criteria used to determine whether the EBS is functioning as designed are presented in Sections 4.4.2 and 4.4.3 of the 2016 Year 22 Data Monitoring Report.

#### 1.2 Objective

The objective of this assessment is to determine whether the placed EBS-cover material is physically stable and remains at the target cover thickness of ≥ 2 feet. As first defined in the 2011 OMMP, one foot of erosion is generally considered as an indicator of change. The tools defined in the 2011 and 2016 OMMP include bathymetric and aerial elevation surveys, and through-cover coring. Where one foot or greater of target cover is identified, a subjective review of the area of change is used to evaluate significance.

#### 1.3 Background

Construction of the EBS was completed in 2008. Construction included a beach cover system placed on top of contaminated beach sediments and previously-placed habitat fill in the intertidal zone. The EBS extends from the western edge of the Phase II cap west to the former Wyckoff facility property line, and from the berm above the beach to the south, northward to approximately -10 feet Mean Lower Low Water (MLLW).

The cover system consists of a porous geotextile placed on the original beach, a 1-foot-thick layer of 3-inch cobbles placed on top of the geotextile (from approximately +14 feet to -5 feet MLLW), and a 0.66-meter (2-foot) thick layer of fish habitat fill placed on top of the cobble layer. The subtidal cap extension involved the placement of a 1-meter (3-foot) thick layer of sand and gravel covering the subtidal area (to a depth of -10 feet MLLW) immediately north of West Beach and extending up to the southern edge of the existing Phase 1 cap. In this document, the EBS is defined as including both the cover system and the subtidal cap extension.

Long term physical monitoring focuses on the stability of the coarse sand/gravel cover material over the cobble layer. A post-construction "as built" elevation survey was conducted in 2008 by the U.S. Army Corps of Engineers (USACE). The first postmonitoring event on the EBS, conducted during the Year 16 – 2011 monitoring, included a single beam bathymetry survey, a photogrammetric topographic survey, and a limited number of direct hand-measures of the depth-to-cobble layer. The 2011 elevations were compared to the 2008 "as built" conditions.

An evaluation completed as part of the 2012 Year 17 Monitoring Report found that the EBS may not be physically stable with apparent losses of between 1 and 2 feet of material in the lower intertidal zone, and material gains of 2 feet in the upper intertidal zone. Of the direct-cover measurements, all of the low intertidal sampled stations had cover measurements with ≥1 foot of cover thickness. Four stations in the high intertidal area at the upper edge of the fill area had less than 1 foot of cover material (HDR and SEE 2012).

#### Previous Site Elevation Surveys 1.4

Hydrographic surveys have been the main monitoring tool for determining the physical stability of the placed caps at the Wyckoff/Eagle Harbor Superfund site since prior to initiation of the Phase 1 cap construction in 1993. Upland elevation surveys were first added to the monitoring program in 2004. A brief list of the EHOU elevation surveys used in pre- and post-construction monitoring is provided below:

- 1993 1994 cap construction bathymetric surveys included pre-placement condition surveys synoptic with placement activities, and a post-placement survey. These activities are documented in the 1994 On-Scene Coordinator's Report (EPA and USACE 1994).
- 1995 National Oceanic and Atmospheric Administration (NOAA) navigation bathymetric survey (cited in the 1995 Monitoring Report). As the data quality objectives for the NOAA survey differed from those specified in the 1995 OMMP, those data were only qualitatively used in the 1995 (Year 1) Monitoring Report.
- 1995 U.S. Geological Survey (USGS) Subbottom Sonar Profiling, as referenced in the 1995 Monitoring Report.
- 1997 (Year 3) post-placement bathymetric monitoring was conducted solely in the Phase I cap area (SAIC 1998).
- 1999 (Year 5) bathymetric soundings were collected by USACE of the main basin, entrance of Eagle Harbor, and the nearshore areas, including the former West Dock and Wyckoff property shallow subtidal areas (East Beach, North Shoal, and West Beach) (SEA 2000).
- 2004 (Year 8) hydrographic surveys of the main basin and entrance of Eagle Harbor were conducted by the USACE. The nearshore areas surveyed were the same as those conducted in 1999 (Integral and USACE 2004).
- 2004 (Year 8) surveys were subcontracted to APS Mapping and Surveying (APS) for additional shallow subtidal and intertidal soundings in the Phase II and Phase III cap areas as well as the shallow subtidal and intertidal areas surrounding the Wyckoff facility (Integral and USACE 2004).
- 2004 (Year 8) beach elevation surveys were conducted by APS using differential Global Positioning System and traditional range-azimuth survey techniques. A 7-acre upland area was also surveyed as part of the February 2004 study (Integral and USACE 2004).

- 2005 photogrammetric topographic survey was conducted on 1 September 2005, and a bathymetric survey was conducted 26-27 September 2005. These surveys were merged together to create the 2005 combined detailed elevation model surface cited in the 2011 Year 17 Monitoring Report (HDR and SEE 2012).
- 2008 EBS post-construction ("as-built") single beam hydrosurvey (HDR and SEE 2012).
- 2010 bathymetric soundings for the entirety of the EHOU were collected by USACE. This included all of the Eagle Harbor Basin, West Beach, North Shoal, and the nearshore area of East Beach (HDR and SEE 2012)
- 2010 on-land elevation survey data were collected using photogrammetric mapping methods by APS. The combined bathymetry and elevation survey data were used to determine areas of erosion and accretion on the EBS (HDR and SEE 2012).

#### 2 Methods

Methods for the site elevation surveys are described in the 2016 Field Sampling Plan (FSP) of the Quality Assurance Project Plan (QAPP), (Appendix B of the primary report to which this appendix is attached). Physical stability measurements outlined in the 2016 OMMP Addendum included a hydrographic survey, aerial image and lidar acquisition, and direct physical measurements of the cover thickness at select locations.

Elevation mapping was led by Miller Creek Aerial Mapping (MCA); the survey team included TerraSond (bathymetric surveys), APS Surveying and Mapping (field surveys), GeoTerra (airborne lidar acquisition), and GPS Surveying (aerial imagery acquisition). Direct field measurements of the EBS cover thickness, conducted by HDR, with Science and Engineering for the Environment, LLC (SEE), the U.S. Environmental Protection Agency (EPA), USACE, and the Washington State Department of Ecology (Ecology), are reported in Section 3.3 of the Year 22 Data Monitoring Report.

Methods for the elevation surveys are briefly discussed in the following sections.

#### 2.1 2017 Bathymetric Surveys

The bathymetric survey was conducted following the methods described in the FSP. One significant change is that Year 22 bathymetric data was collected using both single beam sonar, and also using multibeam sonar. The previous surveys had been conducted with single beam; future bathymetric monitoring at the EHOU will be completed using multibeam. The objective of the concurrent sonar measurements was to document the similarities and differences on shore profiling using the two methods.

Bathymetric data were collected on 11 January 2017 between 12:00 – 16:00 PDT on a rising tide to 11.97 feet MLLW at 15:02 hours. Surveys were conducted from the TerraSond survey vessel R/V Carta. A complete description of the methods, survey control points, quality assurance and quality control measures, and data processing, are provided in the TerraSond survey report in Appendix I-1.

The deliverables provided in Appendix I-1 include the following:

- Appendix I-1a. TerraSond Eagle Harbor project report
- Appendix I-1b. ASCII X,Y,Z point files of bathymetric points. Gridded at 1 foot x 1 foot (electronic only)
  - Multibeam files are noted with a MBES
  - Single beam with a SBES.
- Appendix I-1c. Shaded-relief imagery of multibeam data in GEOTIF format (TIF/TFW) (electronic only)

#### 2.2 2017 Beach Elevation Surveys

The orthophoto and lidar surveys were conducted following the methods described in the FSP. Details of both surveys are included in the MCA elevation surveys report (Appendix I-2), but are described briefly here.

The orthophoto of West Beach was collected on 30 January 2017 using a gyro-stabilized Ultracam Falcon digital image sensor mounted in a Cessna 206 StationAir. Imagery was acquired under high overcast conditions to minimize shadows. Orthophotos are provided in Appendix I-2, and include both Red/Green/Blue (RGB) color, and color infrared images.

As a result of a combination of operational difficulties, inclement weather, and a lack of daylight low tide sequences, it was not possible to obtain the lidar until late spring 2017. The lidar data was acquired on 26 May 26 2017 during a single mission. The sensor used was an Optech Galaxy mounted in a Cessna 310 fixed-wing aircraft. The flight plan was designed with a minimum of 50 percent overlap in swath footprint to minimize laser shadowing and data gaps. The lidar data was acquired with a planned nominal density of >8 points per square meter and during a -2.6 feet MLLW tide to ensure significant overlap between the lidar and hydrographic data.

The deliverables provided in Appendix I-2 include the following:

- Appendix I-2a. MCA Orthophoto, Lidar, and Bathymetric Survey Report project report
- Appendix I-2b. RGB and infrared color orthophotos (electronic only)
- Appendix I-2c. Lidar data including (electronic only):
  - All returns
  - Bare earth returns
- Appendix I-2d. Digital Elevation Model (DEM) (electronic only)

#### 2.3 Interpolation Methods

The 2017 elevation and bathymetric data were prepared by MCA and TerraSond. Delivery reports for these datasets are included in Appendix I-1 and I-2. DEMs for each dataset were generated and provided by MCA. One combined lidar and bathymetry DEM was also provided. No interpolation of surface values was performed as these combined datasets provided full coverage of the EBS. HDR reviewed the combined dataset and confirmed multibeam bathymetry data were used and was supplemented by the lidar to

provide full coverage of the EBS. HDR also spot checked the merged edge elevation values against the original DEMs.

To compare elevation values between survey data across different years, the ArcGIS Raster Calculator was used to subtract the elevation values of the most recent year's data (i.e., 2017) from the corresponding elevation values of previous years. The resulting output provided values indicating the change in elevation between the two years.

Raster datasets were displayed using 14 manually-defined display classes. Classes were specified at 1-foot intervals, with an additional interval specified at 0.5 and -0.5 feet, respectively to better illustrate small changes in the surface elevations.

Elevation profiles were generated by first creating regularly spaced points at 10-foot intervals along specified transects. Elevation values from the combined elevation dataset for each of the time periods evaluated were transferred to the corresponding transect point using the Extract Values to Points tool. The resulting dataset was imported into Microsoft Excel and charts generated comparing the extracted elevation values between years.

# 3 Results

# 3.1 Single vs. Multibeam Bathymetry

The single beam and multibeam data in the Wyckoff/Eagle Harbor Superfund site surveys showed good correlation (Figure I-1). To generate the comparison in Figure I-1, the single beam and multibeam xyz data were brought into AutoCAD Civil 3D 2013. Five profile lines, spaced across the survey from east to west, were drawn in AutoCAD and the single beam versus multibeam surface elevations were compared along these lines. Figure I-1 presents one of those five profiles between the two surveys.

The single beam and multibeam generally found to be within 0.1–0.2 feet of one another. Measurements with the multibeam tend to report lower elevation than the single beam. Based on this relatively tight comparability, coupled with the fact that the sounding data density was significantly higher using multibeam, the multibeam surveys data were subsequently used to make comparisons to the 2009 and 2011 data sets used for comparison to the 2008 "as built" EBS condition, and the 2011 monitoring data.

# 3.2 Elevation Survey Findings

#### 3.2.1 Elevation Contours

Elevation contours in 1 foot increments within and proximal to the EBS, based on the combined lidar and bathymetric data sets, are shown in Figure 1-2. The boundaries of the EBS extend from approximately +15 feet MLLW to between -12 and -14 feet MLLW. This is consistent with the presentation of the EBS elevations in the 2011 Data Monitoring Report (HDR and SEE 2012). At the west edge of the EBS, formation of a sand spit is evident; the leading edge of this feature is at approximately 0 feet MLLW.

An additional advantage of using the multibeam is the ability to be able to generate shaded relief elevation maps (see Figure I-3). Referred to in the TerraSond report

(Appendix I-1a) as a "sun illuminated imaging," TerraSond used the software Caris HIPS to create a 3D effect of inserting a shadow onto the multibeam base surface for the georeferenced orthophotograph. Figure I-3 presents the visualization of the subaquatic seafloor.

The sand spit is more clearly seen in the shaded relief elevation map (Figure I-3). The sand spit, not observed in the 2011 survey, is evidence that sand is being mobilized from the EBS, translocated along the shore and depositing onto the spit.

The multibeam data revealed in-water structures that had not been observed or reported in any of the previous surveys. These underwater structures, while off the EBS, are on the Phase I cap (see Figure I-3). Shown in a color relief inset box on Figure I-3, structure numbers 1 through 3 appear to be objects placed on the cap; structure number 4 appears to be sunken logs.

#### Changes in Elevation - 2008, 2011, and 2017 3.2.2

To evaluate the subtidal cap stability, the results of the 2017 survey program were compared to surveys previously completed in 2008 (post-placement) and 2011. Topographical survey data from the elevations surveys in 2008 and 2011 were combined by USACE for the 2011 Year 17 Monitoring Report into a survey grid; those grid files were provided to HDR. Differences in elevation were determined by subtracting each year's grid elevations from previous monitoring elevations as follows:

- 2008 to 2011 (Figure I-4)
- 2011 to 2017 (Figure I-5)
- 2008 to 2017 (Figure I-6)

Figure I-4 compares the 2008 post-construction elevations with the elevation survey monitoring completed in 2011. Figure I-4 is the same as Figure 3-5 in the 2011 Year 17 Monitoring Report. The 2011 Year 17 Monitoring Report noted that both erosion and accretion occurred at the EBS between 2008 and 2011. Within the lower intertidal areas, an apparent loss of between 1 foot and 2 feet of cap elevation was identified, while in the high intertidal, gains of up to 2 feet of new material were noted. Comparisons of elevations for beach profile transects for 2008 and 2011 are also shown on xy plots in Figure I-4. In all of those plots, the 2011 elevations are either at or below those measured in 2008. USACE calculated that approximately 5,005 cubic yards of material had been lost from the EBS between construction and 2011.

Figure I-5 compares the 2011 and 2017 monitoring elevation surveys. This comparison suggests that substantive erosion is still occurring in the lower intertidal and subtidal sections of the EBS; between 1 foot and >5 feet of material loss. Of specific note is the high intertidal region between beach transect lines 4+00 and 6+00, where 1 to 3 feet of erosion is indicated. This is the same area of the EBS where the direct cover measurements reported in Section 3.3.2 of the 2017 Data Monitoring Report showed that

<sup>&</sup>lt;sup>1</sup> The elevation contour color scheme presented in the 2017 legend bar is changed from the scheme used as part of 2011 reporting. The 2011 figures represented elevation losses in shades of blue, and elevation gains in yellows-to-red. For ease of identifying areas of erosion, the color scheme is reversed here: yellows-to-red represent erosion; areas of blue represent accretion.

no (0 feet) cover material remained; the underlying cobble area was visible. It is worth noting that this specific area is proximal to the outflow pipe that channels stormwater from the hill above onto the beach. Other than that specific area, the beach profile transect plots suggest that for the upper intertidal areas little to no elevation change is evident.

Figure I-6 compares the 2008 post-construction ("as-built") elevations with the 2017 elevations. This figure represents the sum of all elevation changes that occurred since construction of the EBS. Accretion of material is shown in the uppermost intertidal areas just below the berm with substantive losses of between -1 and -5 feet over most of the EBS below approximately the +10 foot contour line. This is further evidenced by the xy beach profile transects on Figure I-6; except for those points above +10-foot elevation, the 2017 points are substantively below the 2008 post-construction surface elevations.

#### 3.2.3 EBS Field Cover Measurements

The direct field-cover measurements on the EBS are discussed in Section 3.3.2 of the 2017 Data Monitoring Report, and are briefly represented here to support the physical stability evaluation. The direct hand-measurements of the EBS cover in 2017 show mixed findings (see Figure I-7). Of the 12 measurements made on the EBS during the 2017 monitoring, seven stations had ≥2 feet cover material, two stations were approximately between 1 and 1.5 feet, and three stations had 0 feet of cover material. The area where no cover material was identified is in the upper intertidal area of grid H12; at this location the underlying cobble was visible.

That erosion is occurring is indicated by the fact that the corresponding cover measurements made in 2011 were greater than that observed in 2017 (Figure I-7). This is especially noted at the measurements made in the upper intertidal grid H12 where approximately 1 foot or greater of cover was identified in 2011, whereas in 2017 no cover material was identified and the underlying cobble is directly exposed. Further evidence of erosion was found at the following 2017/2011 paired measurement locations: I12-c2, a 2-foot elevation loss; H12-a2, a 0.65-foot loss; and F12-d1, a 1.6-foot loss.

# 3.3 EBS Physical Stability Evaluation

The surveys discussed in this technical memorandum were undertaken to determine whether the EBS is physically stable and remaining in place at the target cover thickness. The survey data suggest that the EBS cover material is not physically stable, in some areas has less than the target cover thickness of ≥2 feet, and is below the minimum of 1 foot of fish habitat mix material that may trigger additional actions. Data supporting that finding are those listed below.

<u>2008 to 2017 Elevation Change</u>. Loss of elevation, relative to the 2008 "as-built" survey, is evident across the EBS (Figure I-6). With the exception of the upper intertidal where some accretion appears to have occurred, on average >1 foot of erosion across the EBS is apparent. The four beach profile transects shown on the right column of Figure I-6 demonstrate that the 2017 elevations are less than the 2008 as-built survey elevations. This finding is consistent with 2011 where, for these same four transects, the 2011 elevations were generally less than the 2008 as-built elevations.

Figure I-8 presents a graph that provides a comparison of the erosion/accretion along the four beach transects, comparing the 2008 to 2011 (blue line), 2008 to 2017 (red line), and 2011 to 2017 (green line) survey information. In the graphs, "0" on the y-axis represents the 2008 condition, values below the 0-line represent erosion, and values above the 0-line represent accretion. What is evident on the graph is that erosion is principally occurring in the lower intertidal and subtidal areas of the EBS. These graphs also indicate that most of the changes in elevation occurred in the period postconstruction to the 2011 monitoring, but that erosion is still occurring.

**Direct Measures.** That erosion may still be ongoing is indicated by the fact that the corresponding cover measurements made in 2011 were greater than those observed in 2017 (Figure I-7). This is especially noted at the measurements made in the upper intertidal grid H12, where in 2011 approximately 1 foot or greater of cover was identified, whereas in 2017 no cover was observed and the underlying cobble is directly exposed.

Additional Observation. The observation of the formation of a subtidal sand spit (Figure I-3) at the western edge of the EBS is evidence that cross-shore sorting (erosion) and long-shore transport of the finer sand is occurring.

#### **Uncertainty Evaluation** 3.4

That erosion is occurring on the EBS is evident in the lines of evidence cited above. What is uncertain is the degree to which that erosion has occurred across the entire EBS, and the degree to which it is ongoing. Two principal sources of uncertainty exist relating to the evaluation of physical stability of the EBS: (1) completeness and comparability of the data underlying the interpolations for the 2008, 2011, and 2017 surveys, and (2) whether the remaining cover on the EBS as a whole is less than 2 feet in depth.

The first source of uncertainty in this interpretation may be in part due to the differences in the spatial comparability and coverage (completeness) of the data points in the three rounds of surveys. The underlying elevation data for the 2008 and 2011 interpolations were completed by comparing single beam bathymetry and photogrammetry, whereas the 2017 data comparisons used multibeam bathymetry and lidar. The analysis of single beam versus multibeam bathymetry data completed by TerraSond demonstrated the relative comparability of the two measurement methods at the same point (Figure I-1). However, the multibeam data are on a finer spatial resolution, with 5 data points per square foot over the entire survey area, whereas the single beam data are on transects spaced approximately 160 feet apart and data points spacing slightly over 1 foot.

Data coverage in at least the 2008 and 2011 surveys was incomplete for much of the intertidal zone on the EBS. The 2008 as-built survey data are based solely on hydrosurvey data; no corresponding photogrammetry data was collected to provide upper intertidal elevations. In 2011, the bathymetric survey only went shoreward up to between -0.4 feet MLLW and -5.9 feet MLLW. The 2011 aerial photogrammetry data points were sparse on the EBS and only extended to +10 feet MLLW (see Figures 2-1 and 2-2 in the 2011 Year 17 Monitoring Report). By contrast, the 2017 lidar and bathymetry data overlap is down to -2.6 feet MLLW on the lidar and up to +4 feet MLLW for the bathymetry data.

The second source of uncertainty on the physical stability of the EBS rests with the limited number of direct-measurements of cover thickness. The complete erosion of the EBS cover in the upper intertidal areas of grid H12 (see Figure I-7) is paired with the fact that in the lower intertidal measurements in H12 still had ≥ 2 feet of cover. What is not evident from the elevation surveys is whether the EBS cover material is less than 2 feet of thickness in the areas of apparent erosion.

#### Conclusions 4

Collectively, the lines of evidence point to ongoing physical instability of the EBS cover material. Substantive erosion is shown in much of the EBS between post-construction (2008) and 2017. In some places, no cover is observed and the underlying cobble armor layer is exposed. The data suggest that erosion is ongoing and may not have stabilized. This conclusion is tempered however with considerable uncertainty relative to the comparability of the elevation survey data between the monitoring years, and by the fact that very limited direct-measurement data exists on EBS cover thickness.

While EBS maintenance actions appear to be warranted, the fact that the EBS cover remains an effective barrier to non-aqueous phase liquid seeping and contaminant advection, and is a functioning habitat for benthic invertebrates (see Section 4.4 of the 2017 Data Monitoring Report), it would be appropriate to further evaluate the relative physical stability of the EBS before making any construction-related maintenance decisions.

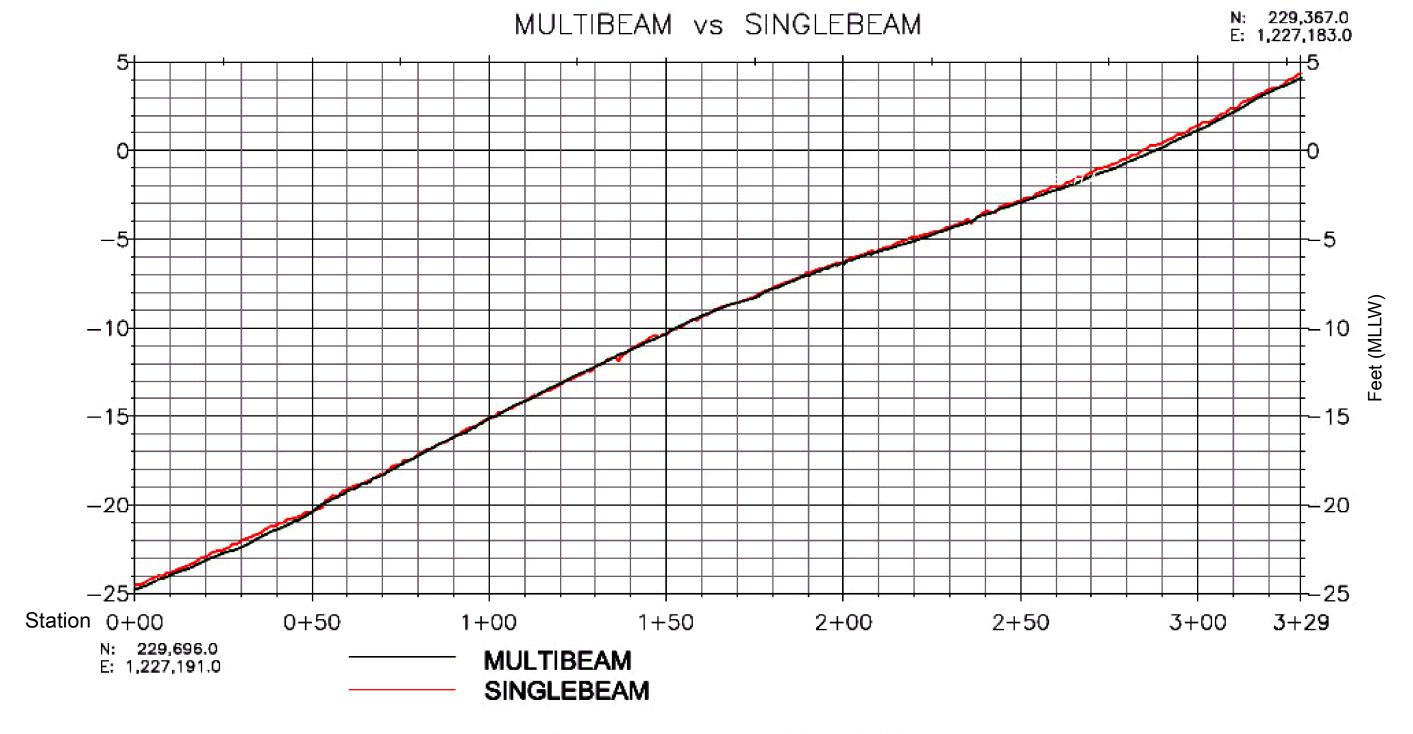
Specific recommendations for follow-up monitoring include:

- A systematic direct-measurement evaluation of the EBS cover thickness following the same methods used in this 2017 Data Monitoring Report. At a minimum, establish complete east-west transects on 5 foot contour intervals (e.g., +10 to +15, +5 to +10, 0 to +5, and -5 to 0 feet MLLW) and take measurements every 50 feet (for a total of 20 cross-transect measurements).
- Conduct additional comparisons between the methods used across the three different survey events to determine the actual degree of uncertainty associated with the elevation comparisons.
- Conduct an additional multibeam and lidar survey at a minimum one-year after the 2017 bathymetric survey. Compare the resulting data to the 2017 data to determine if further erosion has occurred.
- During the upcoming 2017-2018 winter rain storms, physically inspect the EBS to evaluate the stormwater outflow including measures of flow, direction of flow, and any evidence of erosion due to the outflow.

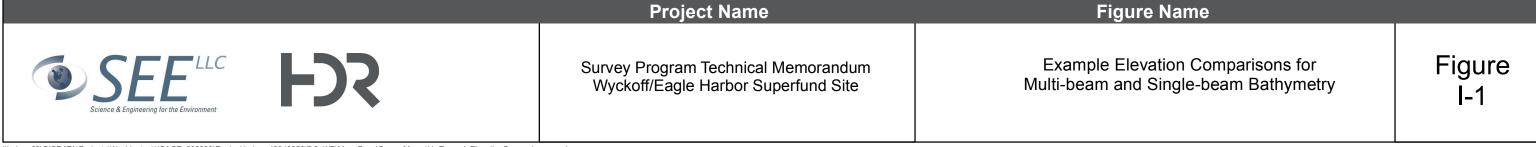
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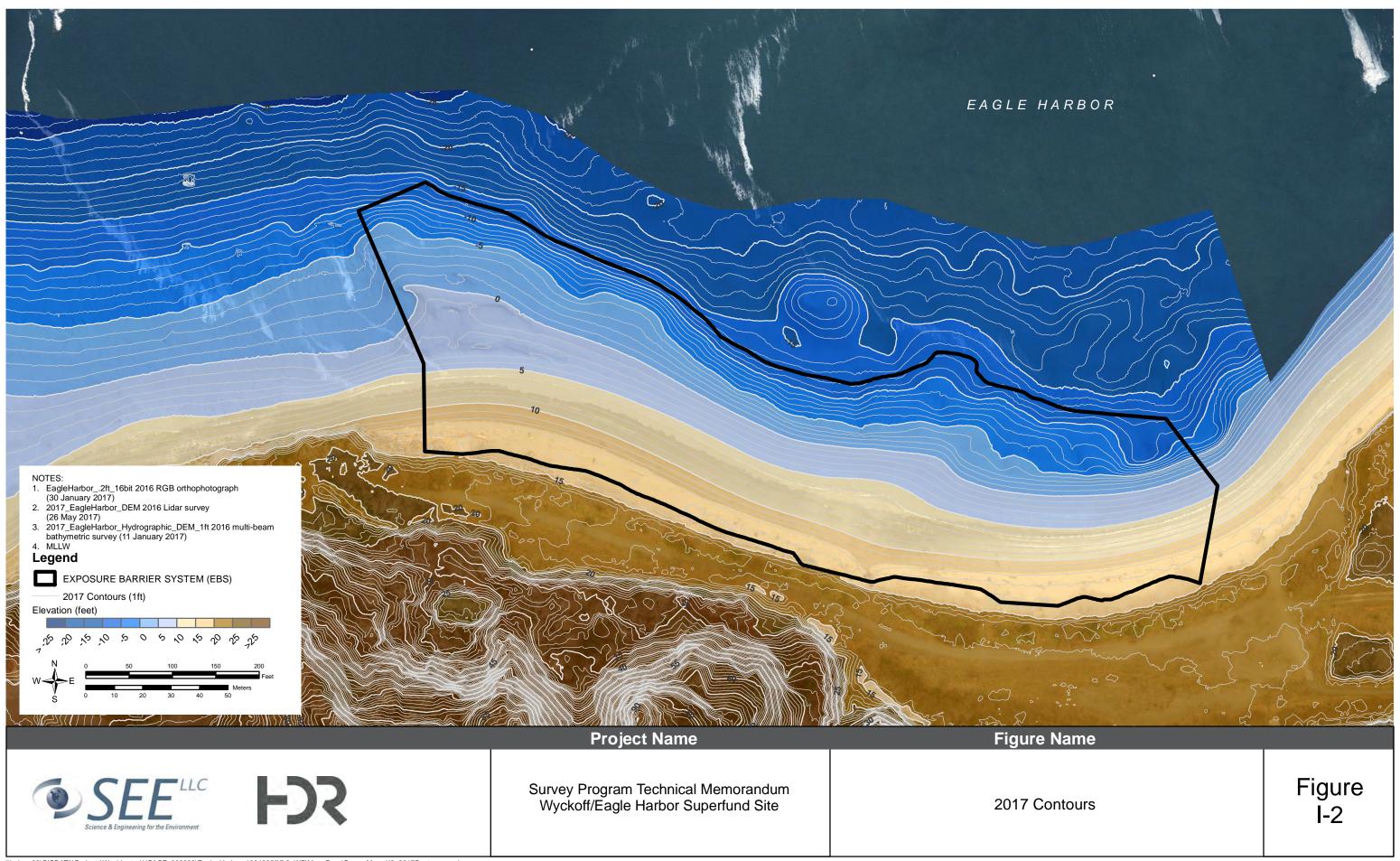
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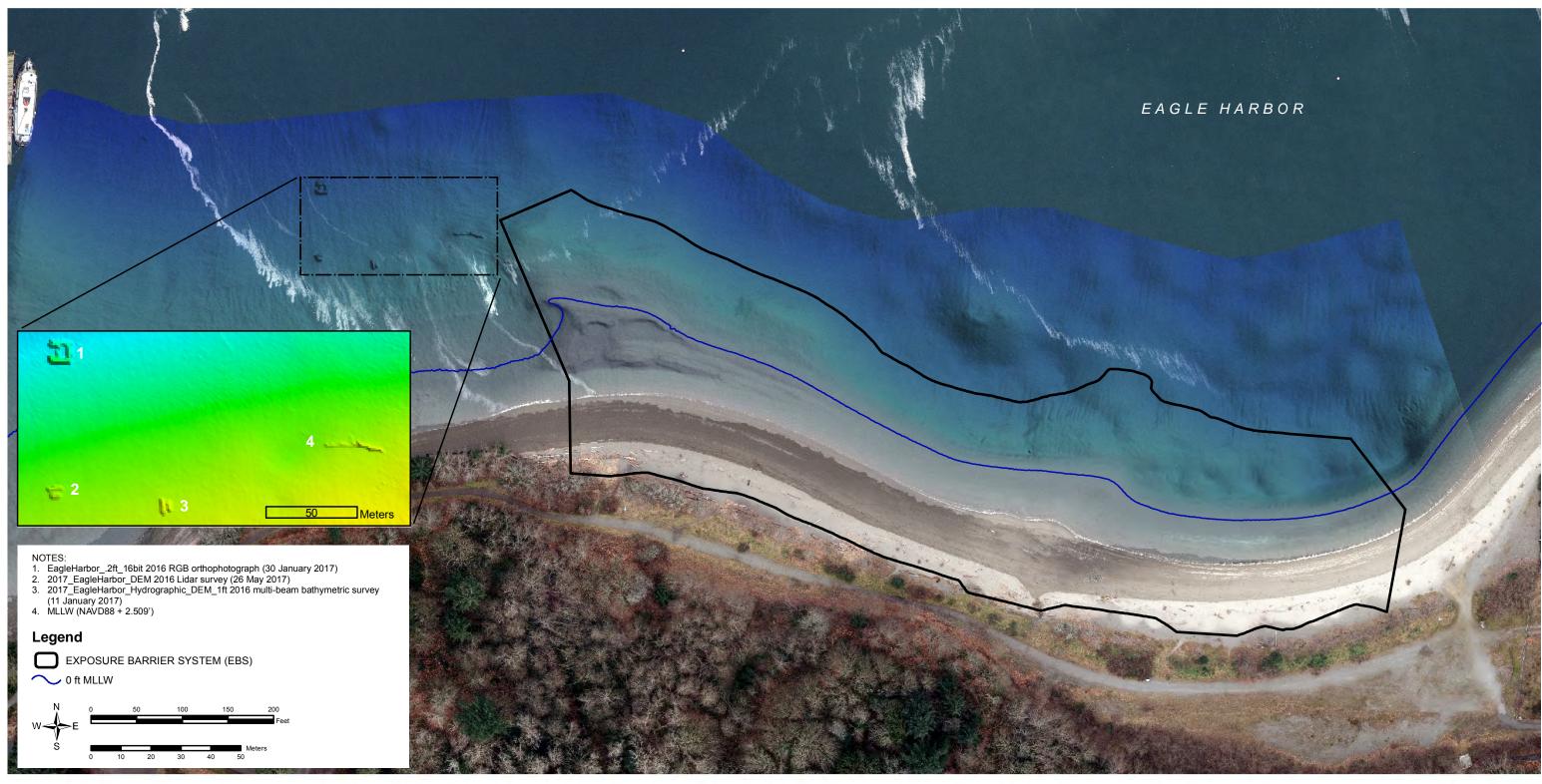
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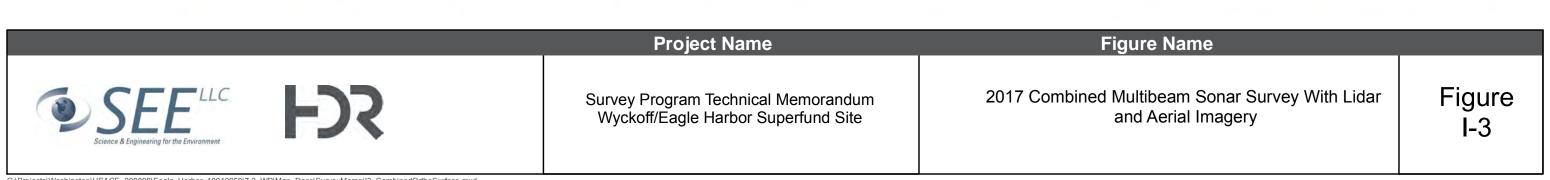


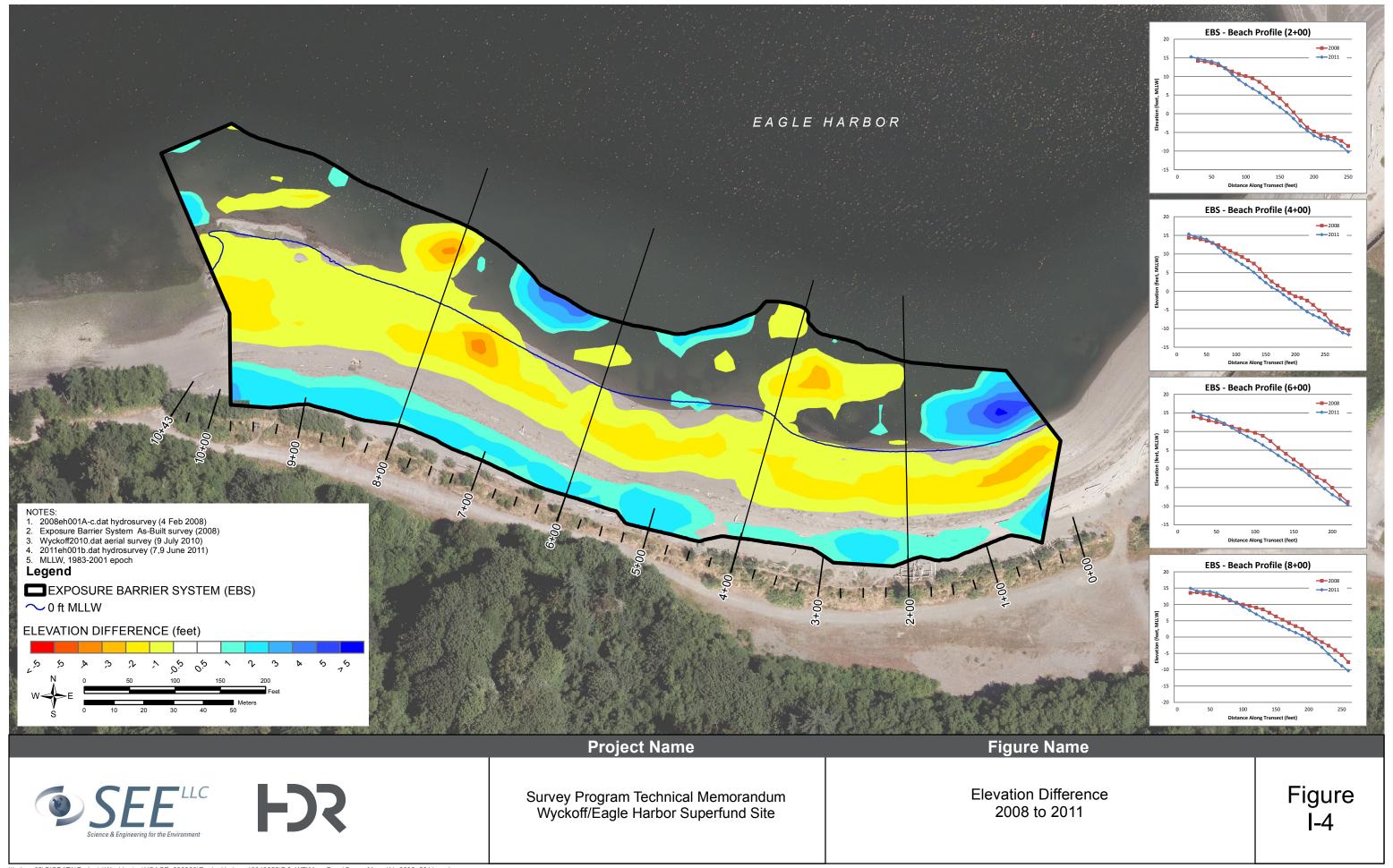
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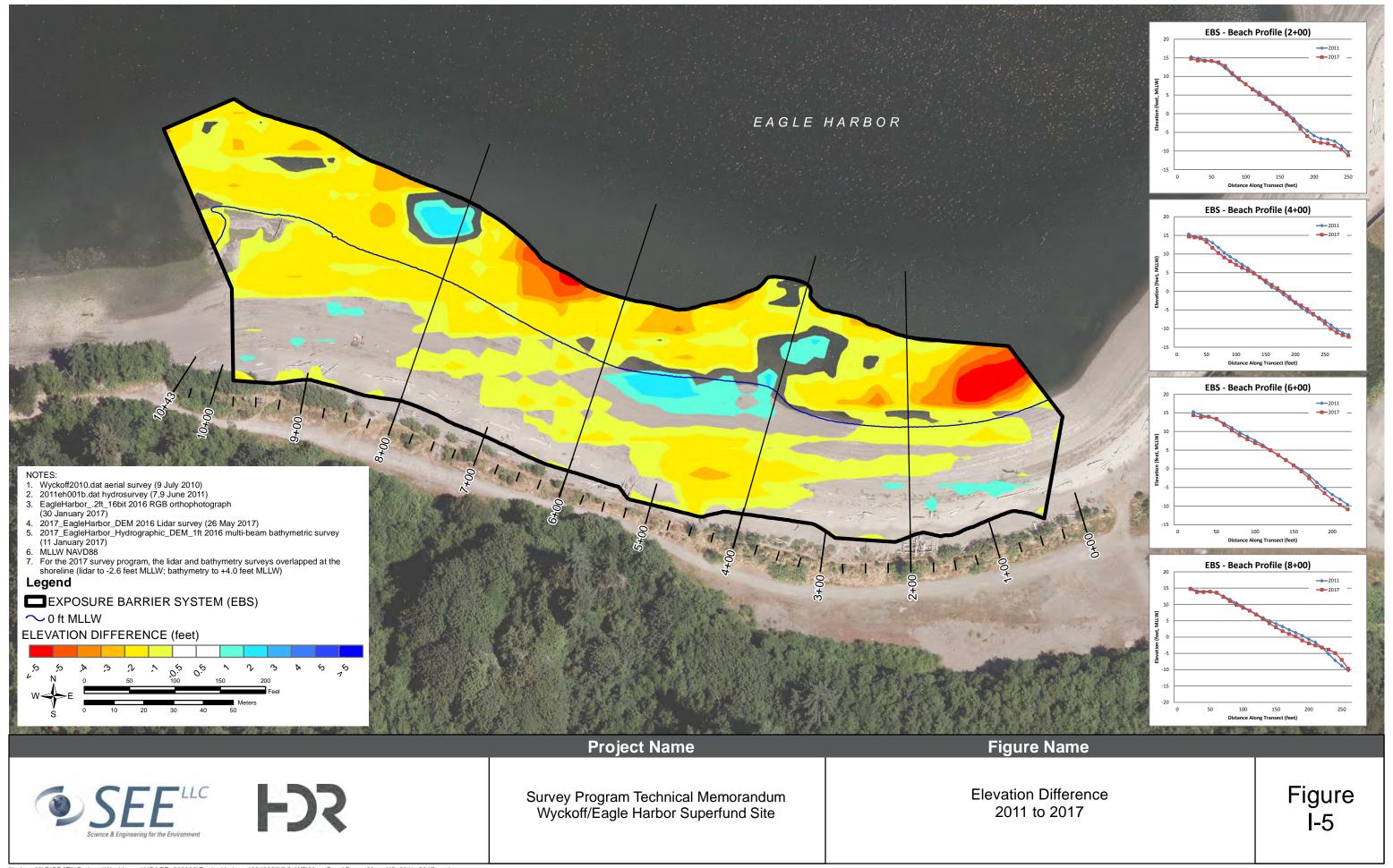


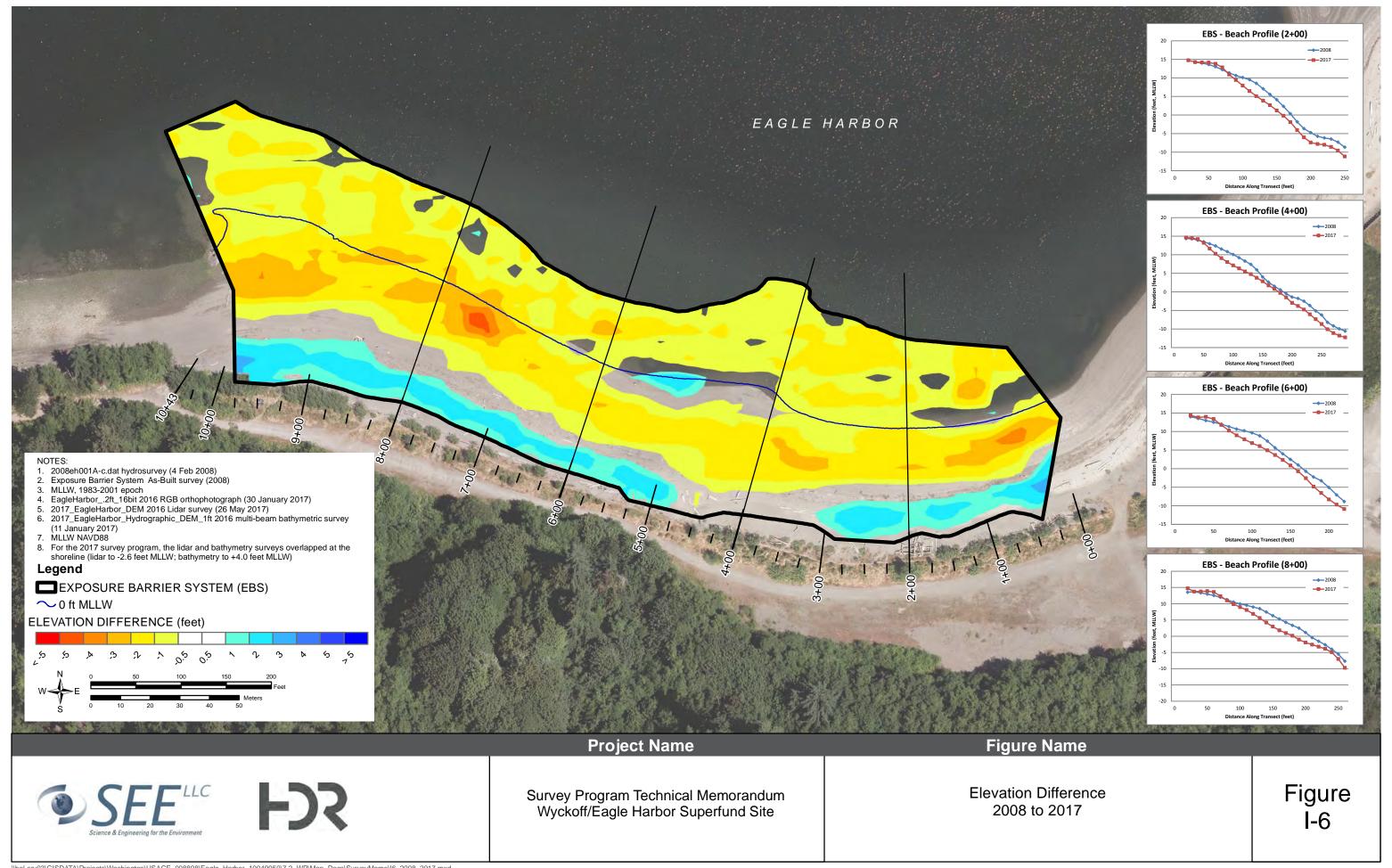




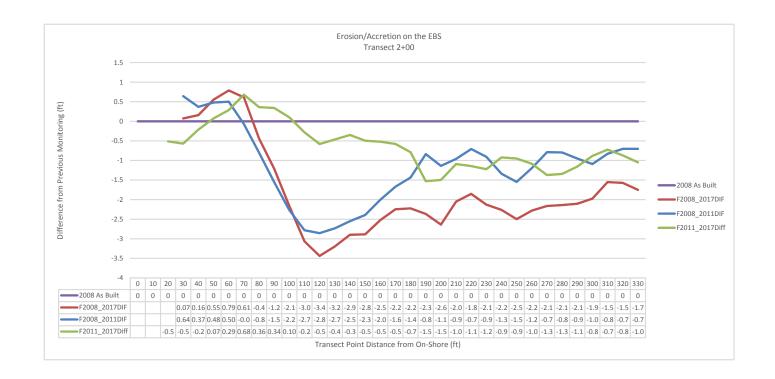


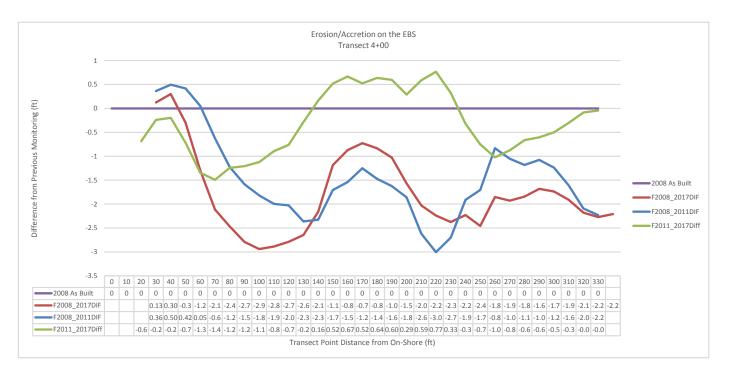


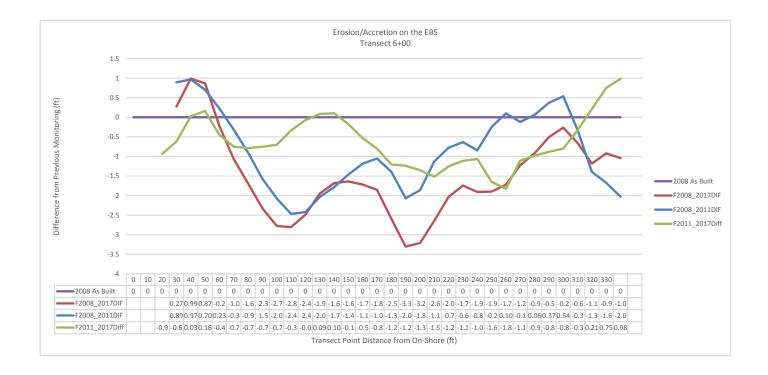


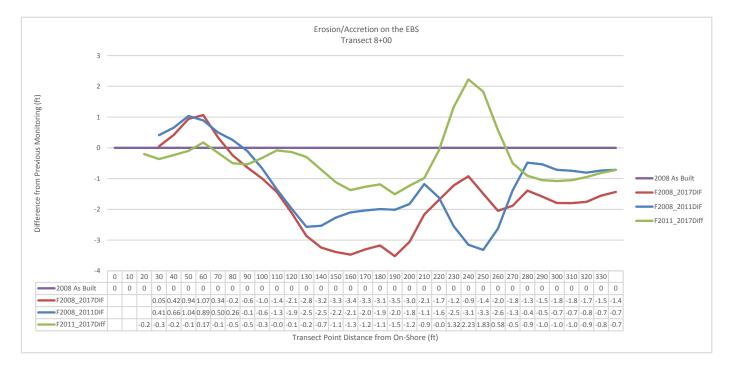


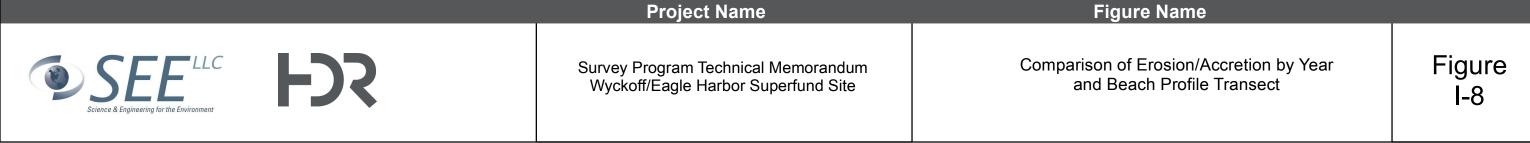




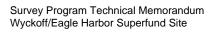








# Appendix I-1a. TerraSond Eagle Harbor Project Report



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# **Project Summary**

TerraSond, Limited performed multibeam and single beam hydrographic surveys at Eagle Harbor offshore of Bremerton Island, WA. The field survey took place January 11, 2017. The survey area is shown below. Coverage extends to as near to shore as was safely navigable.

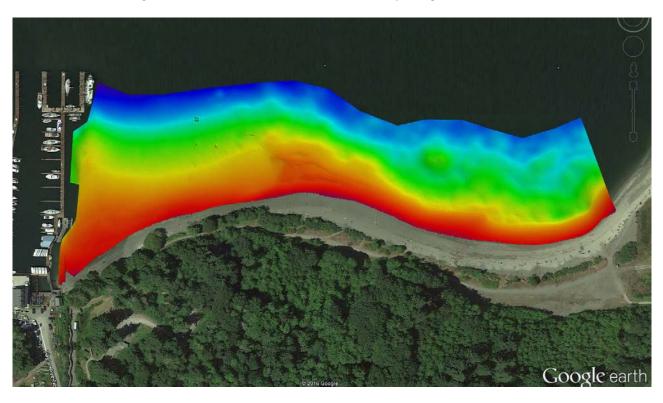


Figure 1 - Survey Area

# **Survey Control**

#### **Datums**

#### **Horizontal Datum**

The survey data was collected using Washington State Plane North Zone NAD83 (2011) in US Survey Feet from the TerraSond Office base station. The final deliverables were completed in Washington State Plane North Zone NAD83 (91). A shift was computed using 3 monuments in the area to determine the horizontal difference at the project site between NAD83 (2011) and NAD83 (91). This difference was then applied to each point set. The average used in the calculations was 0.374 USFT in X and 0.345 USFT in Y.

#### **Vertical Datum**

Survey Data was collected on the ellipsoid from the TerraSond Office base station, the base station equipment is a Trimble Global Positioning System (GPS) model NetRS. The NAVD88 (North American Vertical Datum of 1988) Height was computed for both the single beam and the multibeam data by applying Geoid 12A during data processing. The Mean Lower Low Water (MLLW) values were computed





using the difference from the Washington State Department of Transportation (Wash DOT) monument IS1825 and Monument ID5139.

Wash DOT IS1825 NAVD88 Elevation 18.261 US FT MLLW Elevation 20.77 US FT Difference applied from NAVD88 to MLLW 2.509 US FT

Table 1 - Control Checks

Station		Northing	Easting	Elevation (NAVD88)
IS1825	REC	231634.58	1226908.01	18.26
IS1825	Check	231634.61	1226908.15	18.34
IS1825	Check	231634.60	1226908.19	18.31





Figure 2 IS1825 Looking southeast and IS1825 monument



# **Survey Equipment**

**Table 2 - Survey Equipment** 

Component	Model	Description
Multibeam Echosounder	R2 Sonic 2024	400kHz multibeam, 0.5 degree beamwidth.
Single beam Echosounder	Odom EchoTrac	Dual Frequency, 3° single beam puck
Inertial Navigation System/RTK GPS	Coda F185	Position, heave, pitch, roll and heading sensor.
Real Time Kinematic (RTK) Base Station	Trimble R8	Dual frequency, low-latency base GPS receivers.
Sound Velocity Profiler	AML Minos X	Internal recording, 500dBar instrument for measuring sound velocity profiles.
Acquisition Software	QINSy 8.1	Hydrographic data acquisition and navigation software.
Processing Software	Caris HIPS 9.1	Hydrographic data cleaning and processing software.

#### Vessel

The vessel used in the survey was the R/V Carta, TerraSond's 27-foot, custom built, shallow draft, aluminum survey platform. The vessel is equipped with an over-the-side multibeam pole mount. The mount has a rotary actuator that swings the pole outboard to deploy the sonar. The pole is bolted into place during the survey. The single beam was mounted in the moon pool at mid-ship and slightly to the port side.

The inertial navigation system used for the survey is a Coda F185. The F185 consists of a motion reference unit (MRU) coupled with two GPS receivers. The MRU is rigidly mounted near the vessel center of gravity, the antennas are mounted port and starboard on the forward cabin roof. The F185 supplies Real Time Kinematic (RTK) position, heading, heave, pitch and roll corrections to the soundings.





Figure 3 - RV Carta



### **Data Acquisition Procedures**

Data was collected on the 11<sup>th</sup> of January, the survey crew started data collection around 12:00 noon local time and ended around 4:00pm. The data was collected in UTC time as seen in the field notes. Single beam lines were run first and then the multibeam lines were acquired.

Hypack 2016 was utilized for acquisition of the single beam data. The software generates a trackline map and displays it over the planned lines to aid the acquisition personnel in determining real time across track error. The tracklines from the June 2011 survey were digitized into AutoCAD and imported into Hypack. These line were driven as closely as possible. A total of 20 single beam survey lines were run.

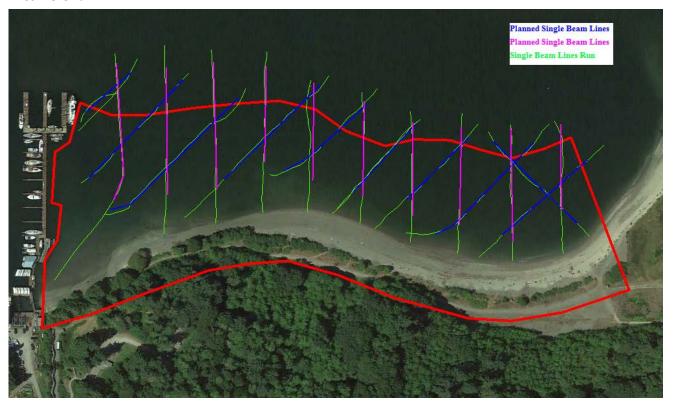


Figure 3 Planned single beam lines in blue and magenta. Single beam lines actually acquired are in green.

QPS QINSy data acquisition software was used for data collection. The software generates a real-time, corrected coverage map of the survey data and quality assurance tools to verify the quality of the data. Line spacing was variable depending on the depths. Generally, the multibeam survey lines were run parallel to the beach and they overlapped between adjacent lines at around 50% of the previous line. Survey speeds were typically 3-5 knots.

A total of three sound velocity casts were taken over the duration of the survey at approximately 2 hour intervals throughout the survey. Sound velocity profiles were used to correct soundings for time-of-flight and beam refraction in post processing.



# **Processing Procedure**

#### **Multibeam Processing**

All multibeam data was processed using Caris HIPS version 9.1. HIPS provides data processing tools that allow you to take all of the raw sensor data recorded during data acquisition and create a final sounding set. The general HIPS workflow is composed of the following steps:

- 1. <u>Data Conversion</u>. Raw data is converted from the native QINSy format to a HIPS format.
- 2. <u>Sensor editing.</u> Sensor data such as heave, pitch roll and navigation is reviewed. The data can be edited for spikes, smoothed, interpolated or rejected if necessary.
- 3. <u>Sound velocity Processing.</u> Sound velocity processing converts the soundings from raw beam angle and time of flight measurements to soundings based on the sound velocity profile of the water column and vessel attitude measurements. Vessel offset parameters computed from patch test results and vessel survey offsets are applied during this step.
- 4. <u>Swath editing.</u> Soundings from individual lines are cleaned in the swath editor. The swath editor allows the hydrographer to examine and reject erroneous data and filter lines based on swath limits.
- 5. <u>Merging</u>. Water level and other vertical corrections are applied to the soundings. The soundings are converted from time, beam and ping format referenced to the vessel location, to a fully geo-reregistered sounding.
- 6. <u>Subset Editing.</u> Subset editing is the final step in the data cleaning process. The subset editor allows the hydrographer to view data from multiple survey lines in a region in a single 2D and 3D spatial editor.
- 7. <u>Surface Processing.</u> After the data has been cleaned and finalized, HIPS creates a gridded surface from the data called a base surface. The horizontal resolution of the surface is user specified and depends on the resolution of the acquired data and the accuracy requirements.

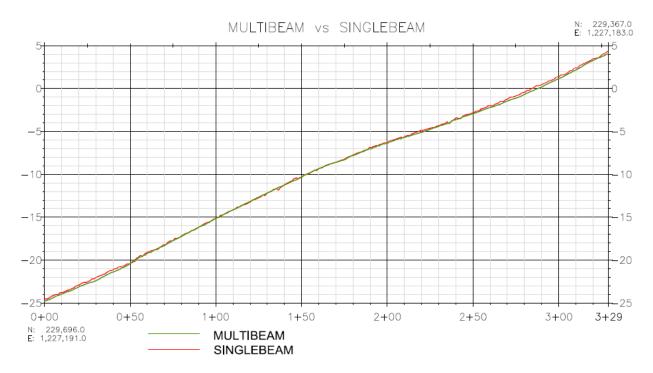
#### **Single Beam Processing**

All single beam data was processed using Hypack 2016 Single beam editor. The echogram was loaded into Hypack and the sounding values compared to the echogram. Soundings were interpolated based on the echogram comparison. The final points were exported into ASCII as a 1 ft sort.

## **Results**

The multibeam and single beam are within 0.1-0.2 ft in general to one another. The multibeam tends to be lower than the single beam. This data was analyzed by using AutoCAD Civil 3D 2013. The multibeam and single beam xyz data were brought into AuotCAD. Surfaces were created for each data set. 5 profile lines, spaced across the survey from east to west, were drawn in AutoCAD and the surfaces compared along these lines. A representative profile between the two surveys is shown below.





NOTE: VERTICAL EXAGGERATION IS 5X

Figure 4 Multibeam and single beam comparison

The crossline comparison for the single beam data against itself compared well within the expected parameters for a single beam survey. Each intersection was visually compared in the software program Hypack 2016. A typical cross section is seen below.

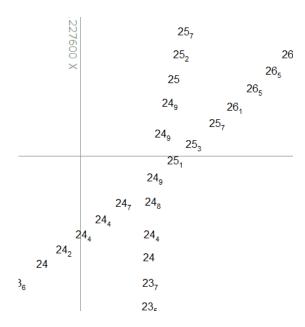


Figure 5 Single beam crossline intersection. Soundings in feet.

# **Quality Control Checks**

Prior to surveying, during data collection and in post processing, a series of quality assurance checks were conducted to verify the sounding accuracies. The checks that were conducted included:

- 1. Control Check (Described in Survey Control Section)
- 2. Bar Check
- 3. Lead Line Check
- 4. Patch Test

#### **Bar Check**

A bar check was conducted to verify sonar sounding accuracy and the vertical offsets applied in post processing. A bar was lowered below the sonar and multibeam raw files were recorded at each depth. The raw files were processed using the standard processing flow in Caris HIPS. This accounts for all vertical offsets for the positioning and multibeam locations, sonar draft and sound velocity.

Table 4 - Multibeam Bar Check

Bar Depth (ft)	MBES Depth (ft)	Difference (ft)
5.0	4.88	0.12
10	9.94	0.06
15	14.84	0.16
20	19.83	0.17

A single beam bar check was completed at the beginning of the survey and at the end of the survey. The bar started at 10 ft depth and sound velocity set to 4800. The bar was reading deeper than it should have been so the draft was adjusted to 1.2. The bar was then lowered to 30 ft and the nadir depth was reviewed to see if an adjustment was needed to the sound velocity or the draft. The process was checked at the end of the survey with no changes made.

Table 5 - Single beam Bar Check

Bar Depth (ft)	Nadir Depth (ft)	Sound Velocity	Draft	Index
10	10.2	4800	1.3	0
10	10.0	4800	1.2	0
30	30.0	4800	1.2	0

#### **Lead Line Check**

A lead line was utilized to verify that the acquisition software was reading the appropriate depth, it was not used in any calibration procedure. For this survey it is used as a gross error quality check. Lead lines are not overly accurate for two main reasons; the first is that when the lead line is lowered over the side of the vessel it is not on to a flat seafloor so the reading you take off the lead line is different than the sounder reading, the second issue arises when the technician takes the reading off the lead line, they are trying to read the waterline on the tape measure as the vessel moves up and down this creates an error in the measurement as well.

System	Lead Line value	Sonar value	Delta
Single Beam	41.8 ft	41.2 ft	0.6 ft
Multibeam (Port)	38.0 ft	36.3 ft	1.7 ft
Multibeam (Starboard)	35.5 ft	34.5 ft	1.0 ft

#### **Patch Test**

A patch test is a set of systematic lines that are run to determine the alignment errors between the motion reference unit and the multibeam. Roll, pitch, yaw and latency patch lines were run and biases determined using the Caris HIPS calibration utility.

Table 6 – Patch Results

Pitch (deg)	Roll (deg)	Yaw (deg)
-3.800	-1.640	-0.600



#### **Deliverables**

The deliverables provided for this project include: Two sets of data, one overall and one of the inset.

- ASCII X,Y,Z point files of bathymetric points. Gridded at 1ft x 1ft
  - Multibeam files are noted with a MBES,
  - Single beam as a SBES.
- Sun-illuminated imagery of multibeam data in GEOTIF format (TIF/TFW)
  - Wyckoff\_WASPZN\_MLLW\_1ft\_SetRange.tif has a set color range of 0 to +4 mllw as green and +4 to the shoalest sounding as red.
- Project report summarizing data collection and processing procedures.



Project Setup

801 NW 42ND STREET, SUITE 215 SEATTLE, WA 98107 (206) 420-8304 www.terrasond.com

Project Information:				
Project Name:	2017-003 MCA	wackoff.	Date:	
Project Number:	2017-003		JD:	10011
Location:	Eagle Harbor, u	)A		
Personel:				
Position	Name		Company	
Party Chief:				
Lead Hydrographer:	Kathleen Mildon		Terra	Sand
Survey Tech:	Andrew Sondh			
Survey Tech:	Tyler yost		Terro	Sonol
Client:	3			
Client:				
Equipment	T	T		1
N. 14:32	Model Control of the second control of the s	Serial #		Version
Multibeam	R2, Sonic 2024			
Inertial Navigation Positioning	<u>  F185</u>   F185			
Heading	F185 F186			
HPR	F185			
SVP Probe	AMC MILVO SY M	10054		
Acquisition Software	Quest, aps/mbes	Hypack 2	OILA/515	
Coordinate System:				
Horizontal Datum:	Washington Sta	ute Olane Z	one. N	A DODES
Coordinate System:	J		<u>Units</u>	
Vertical Datum:	WAVD88		Units	: <u>F</u> +
Positioning:				
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	Coast Guard DGPS Local Base Station			
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Project Name:	2017-002 MCA WYCKOFF	Date: 1/11/2017
Project Number:	7017-003	JD: OH
Location:	Eagle Harbor	Crew: KM, AS, TY

Conditions	
Weather: 35° F	
Wind: 25 KTS	<u>Seas:</u> > 2 F+
Traffic:	

Draft Measureme	ents WHTE	ZUNL				
Begin Shift	<u>Reference</u>	Ref -Offset	<u>()</u>	<u>WL</u>	MB - Offset	<u>Draft</u>
Port	P2			2.84	-2,06	.78
Starboard	R252			2.81	-2.0 to	.75
End Shift						
Port	100					
Starboard						

Position Check			
Reference Station	on:		
	Record: R8	Measured: (L. ⅓	<u>Delta</u>
Northing:	N: 231293.741	N: 23/293,54	N: 0.20
Easting:	E: 1225098 745	E: 1225028.74	E: 0,0/
Elevation:	EI: 13.110	El:(H1 7.23) 6.02	EI: 0.14

Sound Velocity Cast	S:			
<u>Date</u>	<u>Time</u>	Latitude	Longitude	SV Depth
1/11/17 DIAMIL	19:43	47 37.1	122 31.046	
1/11/17 AWN	21123	47-37.6	230 122°31, <b>04</b> 68 1810 1 22°30, 47	74
111/10 AML	23:57	47257,06	9100 120303	03 <b>5</b>
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Project Name:	MCA wycloff		Date:	1/11/17
	2017-003		<u>JD:</u>	
Location:	lagle has bor	,	<u>Crew:</u>	KM/ASITY
Conditions				-
Weather: 40 +	Lucian O Es			
Wind: Noww		Seas: Flat		
Traffic: No two	whic			
Offsets				
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Bar Check End		1		1
Bar Depth	Nadir Depth	Surface SV	<u>Draft</u>	<u>Delta</u>
10 F+	10 Ft	4800	Draft 1,5	
304	304	4800	Draft 1.	2
Notes:				

Page \_\_\_\_\_\_ of \_\_\_\_\_\_



Project Informatio	n:	
<u>Project Name:</u>	2017-003 MCA Wydeff	Date: 1/11/17
Project Number:	7017-003	JD: 011
<u>Location:</u>	Eagle harbor	Crew: KM/AS/TY

Conditions:		
Weather: 369 F		
Wind: 20 KMS	Seas:	Flat
Traffic: 1000e		

SPES

Survey Lines:					
Line Name	<u>Start</u>	<u>Stop</u>	Speed	<u>HDG</u>	Comment
011-003_20	07. 2007	2009	4,00	185	
011-004-2009	2009	288	7.00	42	latency line
011-005-2001	2011	2012	7, 25	2260	Catendi Lino
1011-003-2014	2014	<b>Z</b> 015	4.00	55	}
011_005-2016		2018	5,00	234	
011_000_202	2021	2023	7	230	
011-007-202	5 2025	2027	7.5	230	
011-028-2009	2029	2030	7.0	236	
011-009-2033	2033	2035	7.0	230	Good Patch area.
011-010-200	2026	2028	7.2	220	
011_011-2040	2040	2041	7,2	235	
011-012-2043		2045	7,2	130	But Sync Erfor Plash
011-001-2047	2047	2.049	65	185	
011-002-2008	2050	2052	6.5	(23)	
011-003-2053	2053	2054	7.0	180	
011-004-2056	7056	2057	7,0	180	
011-000-2059	2059	2:00	7.6	180	
011-007-2102	2102	21:03	7,0	180	Bouyonline
018-009-2105	2105	21:06	7,0	177	7
011-010-2108	2108	21:10	170	174	Posse parch of and 120
011-011-2112	2112	2113	7,0	181	0
01-012-2115	2115	2119	7.5	175	

Notes:
Lead line: 4737,1723N 12231.0418111 echart Depth 41.2 ft
L DEGTO WL 41.8 PT
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Line Notes Page 4 of



Project Name: 2017 - 003 McA wyckoff Date: 1/11/17 Project Number: 2017 - 003 McA wyckoff DDI Location: Eagle harbor Crew: KM/AS/TY  Conditions  Weather: 45° F Wind: 5 Knts Seas: <1ft Traffic: None  Offsets  Antenna ARP to Bottom of Transducer: Antenna ARP to Waterline: Waterline to Bottom of Transducer:  MultiBeam Par Check  Bar Check Begin  Bar Depth Nadir Depth Surface SV Draft Delta  5 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 &
Project Number: 2017-003 Location: Eagle har box Crew: KM/AS/Ty  Conditions  Weather: 45° F  Wind: 5 Knts Seas: <1 Ft  Traffic: None  Offsets  Antenna ARP to Bottom of Transducer: Antenna ARP to Waterline: Waterline to Bottom of Transducer:  Multi Beam Bax Check  Bar Check Begin  Bar Depth Nadir Depth Surface SV Draft Delta  5 £t. 10 £t.
Weather: 45° F Wind: 5 Knts Seas: <1 ft  Traffic: None  Offsets  Antenna ARP to Bottom of Transducer: Antenna ARP to Waterline: Waterline to Bottom of Transducer:  Mutti Beam Par Check  Bar Check Begin  Bar Depth Nadir Depth Surface SV Draft Delta  5 ft, 10 ft,
Weather: 45° F  Wind: 5 Knts Seas: <1 ft  Traffic: None  Offsets  Antenna ARP to Bottom of Transducer: Antenna ARP to Waterline: Waterline to Bottom of Transducer:  MultiBeam Par Check  Bar Check Begin  Bar Depth Nadir Depth Surface SV Draft Delta  5 ft, 10 ft,
Wind: 5 Knts Traffic: None  Offsets  Antenna ARP to Bottom of Transducer: Antenna ARP to Waterline: Waterline to Bottom of Transducer:  MultiBeam Par Check  Bar Check Begin  Bar Depth Nadir Depth Surface SV Draft Delta  5 ft. 10 ft.
Traffic: None  Offsets  Antenna ARP to Bottom of Transducer: Antenna ARP to Waterline: Waterline to Bottom of Transducer:  Waterline to Bottom of Transducer:  Bar Check Begin  Bar Depth Nadir Depth Surface SV Draft Delta  5 \$\frac{1}{2}\$,
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Page 5 of



Project Information	n:	
Project Name:	2017-003 MCA Wyckoff	<u>Date:</u> 1/11/17
Project Number:	2017-003	JD: 011
Location:	Engle Harbor	Crew: KM/AS/TY

Conditions:	
Weather: 45° F	
Wind: 5 KNHS	<u>Seas:</u> <   f-f-
Traffic: none	

Survey Lines:					
Line Name	<u>Start</u>	Stop	Speed	<u>HDG</u>	Comment
0062-MCA				10	Barcheck
0003-MCA	2224	2229			
0004-MCA	2231	2236		/	
40005-MCA	2237	2245		1	Dry Face
5000 6-4CA	2245	2247			
60007-MCA	2248	2249			
0008 -MCA	2250	22			
8 <i>09</i>					
9 10 - MCA	2259	2306			
10 0011_MCA	2306	2318			
110012 - MCA		2370			
12 00 13 - Mca	2321	2323			
13 0014_ Mea	2324	2324			
10015 _ Mca	2324	2325			
150010-Ma	2325	2325			
150017-MCA	2326	232			
10018 Ma	2322	2329			
18 0019 ME	12337	2338			Dutch
19 0620 - ME	2340	2341			patch
= 0021-PATC4	2342	2343			PATCH
00 22 - PATCH	2347	2348			PATCH
20 0023 - PATCH		2350			PATCH
0024 PATCH	2351	2352			PATEL

0024 1774 2351 2352	PATCO
Notes:	<b>"</b> "
Lead Line 38.0 to WL > part of oleph on MBES 36.3	onk leadline 35.5 MRES 34.5
6025 PATCH 2352 2353 00010 PA+CH 2353 2354	
0027 PATICHY 2354 2355 0028 PATCHY 2355 2355	
Line Notes 2000 0003	Pageof



Project Information:					
Project Name:	2017-003	MCA W	uckoff	<u>Date</u>	1/11/17
Project Number:	2017-003		<i></i>		KM, AS, TY
Location:	Eagle how				t.
Coordinate System:					
Horizontal Datum:					· · · · · · · · · · · · · · · · · · ·
Coordinate System:	WASPEN	NAD 2	13	<u>Units:</u>	
Vertical Datum:	WAYD88			<u>Units:</u>	エナ
Station Information:					
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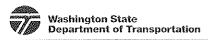
Reciever Type/	Number:		<u>Antenna Type/Nu</u>		
<u>Date</u>	<u>Time</u>	<u>Point No</u>	. Description	<u>HA</u>	<u>Reference</u>
				ad Andreida and Andreida	
				21.00	



Horizontal Control Notes

801 NW 42ND STREET, SUITE 215 SEATTLE, WA 98107 (206) 420-8304 www.terrasond.com

Project Information:					
Project Name: Project Number: Location:	2017-003 A 2017-003 Eagle Nark				1/11/17 KM / AS/IY
Coordinate System:					
Horizontal Datum: Coordinate System: Vertical Datum:	W0SP ZN 88 AVAN	NAD83		<u>Units:</u> <u>Units:</u>	
Station Information:					
	DO DO DISTURE  20 07  H BM-1  SEUCHMARK		Monument Type:  Setting: Stamping:  Latitude: Longitude: Height: Weas, Northing:	WA-Brass of Concretic WIN 1	DOT ap 2 Siclewalk 3M-1
Description:  Base Station Setup:		fand an	Sidewalk	near fe	rng terminal.
Reciever Type/Numb	er:	<u>A</u> 1	ntenna Type/Number:		
Date	Time	Point No.	<u>Description</u>	HA	Reference



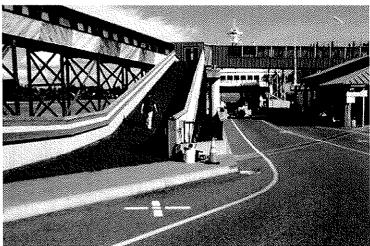
### **Geographic Services**

### SURVEY INFORMATION SYSTEM

### **Report of Survey Mark**

Designation:	IS1825	T.R.S:	25N, 2E, 26	ACCO	UNTS INFORM	ATION
Monument ID:	5139	Corner Code:		воок	PROJECT	INVOICE
NGS Pid:		State Route:		177	XL0903	23-01040
State:	WASHINGTON	Mile Post:		321	MS4466	23-07029
County:	KITSAP	Station:				
Region:	OL	Offset:				
Nearest Town:	WINSLOW	Owner:	GS			
USGS Quad:	BREMERTON EAST	Bearing:	M			

TO REACH THE STATION FROM THE TOLL BOOTHS AT THE WSDOT FERRY TERMINAL IN WINSLOW, GO EASTERLY APPROXIMATELY 100 METERS THROUGH THE VEHICLE LOADING AREA TO MARK ON THE LEFT, IT IS LOCATED IN THE CONCRETE SIDEWALK NEAR THE BASE OF THE PEDESTRIAN RAMP THAT GOES FROM THE LOADING AREA TO THE WOODEN OVERHEAD WALKWAY USED FOR PASSENGER LOADING, 90 CM @ 215 DEGREES FROM A SURVEY MARKER STICKER ON THE EASTERLY POST OF A HENDRAIL SECTION, 34.6 METERS @ 265 DEGREES FROM THE NORTHEAST CORNER OF THE AUTO LOADING RAMP DOCK #1 AND 3.0 METERS @ 130 DEGREES FROM THE APPROXIMATE CENTERLINE OF THE RAMP FOR 'PASSENGER ONLY' LOADING. THE MARK IS AN ALUMINUM SURV CAP CEMENTED INTO A DRILL HOLE AND SET LEVEL WITH THE TOP OF THE CONCRETE SIDEWALK SURFACE.



### **Survey Control**

			Carvey Con				
Datum: NAD 83/0	07		Date: 10/2	21/2008			`
<b>Lat:</b> 47 37 21.593	3595 N Long: 122 3	0 36.897978	W Ellips: -17.	761 (M) -58.2	271 (USFt)	Geoid: -23.32	7 (M)
Washington State	Plane Zone: North		***************************************	<del>"" '"                                   </del>	· · · · · · · · · · · · · · · · · · ·		
Northing		Easting			Scale	Comb Factor	Conv Angle
70602.360 (M) 23	31634.576 (USFt)	373962.31	0 (M) 1226908	.012 (USFt)	0.99997938	0.99998217	-1 14 54.6
Ortho:	Date: 09	9/19/2001	Survey Info	Accuracy	/ Netw	ork N	/lethod
Datum:	NAVD 88		Horizontal	2 CM	SEC	ONDARY C	BPS .
Elevation:	5.566 (M) 18.261 (U	JSFt)	Ellips	5 CM		0	BPS .
			Ortho	1 CM	PRIM	MARY [	OIFF LEVELS
Milw: 1983-2001	6.331 (M) 20.77 (U	SFt)	Milw	1 CM		Ε	OIFF LEVELS

Northing Easting Scale Comb Factor Conv	
	t) <b>Geoid</b> : -23.144 (M)
	.,
70602 268 (M) 231634.274 (USFt) 373962 262 (M) 1226907 855 (USFt) 0 99997938 0 99998214 -1 14 5	Comb Factor Conv Angle
1. 33 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	938 0.99998214 -1 14 54.6
Ortho: Date: 09/19/2001 Survey Info Accuracy Network Method	Network Method
Datum: NAVD 88 Horizontal 2 CM SECONDARY GPS	SECONDARY GPS
<b>Elevation:</b> 5.566 (M) 18.261 (USFt) Ellips 5 CM GPS	GPS
Ortho 1 CM PRIMARY DIFF LEVE	PRIMARY DIFF LEVELS
MIIw: 1983-2001 6.331 (M) 20.77 (USFt) MIIW 1 CM DIFF LEVE	DIFF LEVELS

Datum: NAD	83/91			Date: 09/1	19/2001			
Lat: 47 37 21.	590581 N <b>Lo</b> n	ng: 122 30 3	6.900182	W Ellips: -17.	.578 (M) -57.6	670 (USFt)	Geoid: -23.14	44 (M)
Washington S	tate Plane Zon	ie: North						
Northing		I	Easting			Scale	Comb Facto	r Conv Angle
70602.268 (M)	231634.274 (	JSFt)	373962.26	2 (M) 1226907	.855 (USFt)	0.99997938	0.99998214	-1 14 54.6
Ortho:		Date: 09/19	9/2001	Survey Info	Accuracy	Netw	ork	Method
Datum:	NAVD 88			Horizontal	2 CM	SEC	ONDARY	GPS
Elevation:	5.566 (M)	18.261 (USF	t)	Ellips	5 CM			GPS
				Ortho	1 CM	PRIM	MARY	DIFF LEVELS

### History

Recovered On	Recovered By	Action	Condition
10/21/2008	GEOGRAPHIC SERVICES	UPDATED	•
10/30/2007	GEOGRAPHIC SERVICES	UPDATED	
9/19/2001	GEOGRAPHIC SERVICES	MONUMENTED	



## JOB SAFETY ANALYSIS

# SMALL BOAT AND TRAILER SAFETY

Department Involved: ニスメンソとと、Title of Person Doing Job: Proceed Person Submitting JSA: Roland Poeckert	Manager	Activity Date:   / //   プ   Location of Activity:   その   と   と   と   と   と   と   と   と   と	
Take the tim Remember: This JSA deals with potential hazards or present. If this is the case, the employee must take eliminate or reduce risk.	Take the time to assess all potential hazards. tial hazards expected for the activity outlined. Act is must take appropriate safety measures and doc	ie to assess all potential hazards. Be Aware – Be Alert – Communicate expected for the activity outlined. Actual activity and circumstances may vary and hazards not identified here may be appropriate safety measures and document any changes to the basic job steps, potential hazards and steps taken to	hazards not identified here may be otential hazards and steps taken to
Safety equipment required to do this job:	'n		
Hard Hats	Fire Extinguisher	Work Vest	Dust Mask
Safety Shoes	☐ Safety Glasses w/ Side Shields	☐ Life Rings w/ 90' Floating Line	☐ Back Belts
Hearing Protection	Goggles Goggles	☐ Tag Lines	Face Shield
Gloves Type ( )  Personal Flotation Device (PFD)	Safety Harness Other ( )	<ul> <li>☐ Work Permit Required</li> <li>☐ Lockout/Tagout</li> </ul>	Floor Mat
Comments:			
Description of any other job specific hazards:	ards:		
And the second s	Comments and the comments are comments and the comments and the comments and the comments are comments and the comments and the comments and the comments are comments and the comments and the comments and the comments are comments and the comments and the comments are comments and the comments and the comments are comments are comments and the comments are comments and the comments	WATER TO THE TOTAL PROPERTY AND THE TOTAL PRO	**************************************

10/26/2012

Sequence of Basic Job Steps	Potential Accidents or Hazards	Recommendations to Eliminate or Reduce Potential Hazards
Check boat and secure all equipment on the boat prior to moving	Injury due to slips, trips and falls	Secure any ladders or use a suitable safety ladder for accessing the boat.
	Damage to equipment and other vehicles due to equipment moving and/or falling off boat	Secure all loose equipment using tie downs or stow in an enclosed area.
Check boat and trailer prior to moving	Electrical shock and damage to equipment – boat still connected to electrical outlet (shore power)	Perform a complete walk around inspection to ensure that all electrical connects and lines are safely stored on the boat.
Check tires	Damage to tires and rims if tires not properly inflated	Check tire pressure and correct if necessary.
Check for obstructions	Damage to trailer or boat due to obstructions	Check for and remove any obstructions around and under the trailer.
		Remove access ladders.
		Ensure that trailer is hooked up so that it cannot move when chocks are removed. Remove chocks before attempting to move trailer.

teviewed By:		
Vame (Print): Line 1	Signature:	Date:
Vame (Print): HIMEN SWAM	Signature: A Sauth	Date:
lame (Print): TYUK 4657	Signature:	Date: // / /
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lame (Print):	Signature:	Date:
Vame (Print):	Signature:	Date:



### JOB SAFETY ANALYSIS

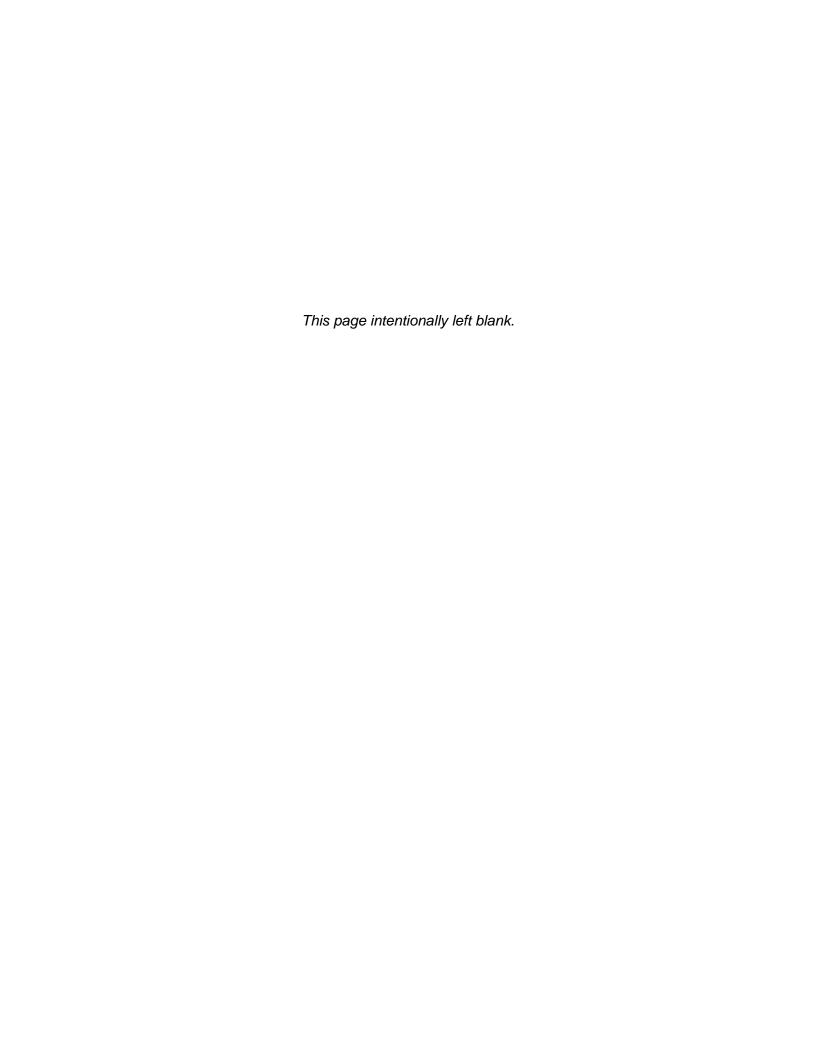
### MAN OVERBOARD RESCUE

Department Involved: <u> </u>		Activity Date: 1/11/17  Location of Activity: Face 1/2 Mox Cox  Supervisor: K, Milder	
Take the time to assess all potential hazards. Be Aware – Be Aiert – Communicate <b>Remember:</b> This JSA deals with potential hazards expected for the activity outlined. Actual activity and circumstances may vary and hazards not identified here may be present. If this is the case, the employee must take appropriate safety measures and document any changes to the basic job steps, potential hazards and steps taken to eliminate or reduce risk.	Take the time to assess all potential hazards. tial hazards expected for the activity outlined. Actu e must take appropriate safety measures and docu	Be Aware – Be Alert – Communicate ual activity and circumstances may vary and ument any changes to the basic job steps, p	d hazards not identified here may be potential hazards and steps taken to
Safety equipment required to do this job:  Hard Hats Safety Shoes Hearing Protection	Fire Extinguisher  Safety Glasses w/ Side Shields Goggles Safety Harness	<ul> <li>Work Vest</li> <li>∑ Life Rings w/ 90' Floating Line</li> <li>Tag Lines</li> <li>Work Permit Required</li> </ul>	Dust Mask Back Belts Face Shield Floor Mat
Personal Flotation Device (PFD)	Other ( )	Lockout/Tagout	✓ 1 <sup>st</sup> Aid Kit
Description of any other job specific hazards:	Captain Sat.	Exes on the perso	Eyes on the person, yell man averlo

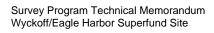
TerraSond Limited Job Safety Analysis

Sequence of Basic Job Steps	Potential Accidents or Hazards	Recommendations to Eliminate or Reduce Potential Hazards
Raise the alarm.	Personnel going overboard trying to attempt rescue.	Keep the person in sight and deploy safety equipment when it can be reached by the person in the water.
	Rescue lines fouling propellers	Never deploy any equipment without informing the bridge.
The Master is to get a Man Overboard (MOB) Fix. The Master	MOB could be lost at sea. It is imperative to establish	It is imperative that MOB has immediate fix and is kept in sight.
will place an "Urgency" (Pan-Pan) Radio call VHF Channel 16 to Notify	communications in work area for immediate assistance.	Knowledge of Emergency Communications prior to work.
the USCG. Alert the Pre-Established Medivac entity including: all other boats in the immediate area.		
The spotter should remain on deck, pointing in the direction of the MOB.	Loose sight of person.	Use as many spotters as available.
Spotter should determine if the MOB is conscious or unconscious.	If MOB is unconscious there could be an immediate drowning situation.	All crews should don their work vest properly to be assured that his head will stay out of water. Depending on the circumstances and conditions other vessels in area that are contacted may recover MOB. It may also
MOB should give an "All Well Hand Wave" if he/she is okay.	There should not be an immediate risk of drowning.	be possible to retrieve cable and use your own ship as a recovery platform as long as MOB can be kept in sight. Other assist vessels in area could definitely perform a quicker rescue if they are present in the
MOB is known to be unconscious.	Immediate risk of drowning.	area. If no other vessels are in the area to assist in the recovery, the decision to sever the deep tow cable is imperative.

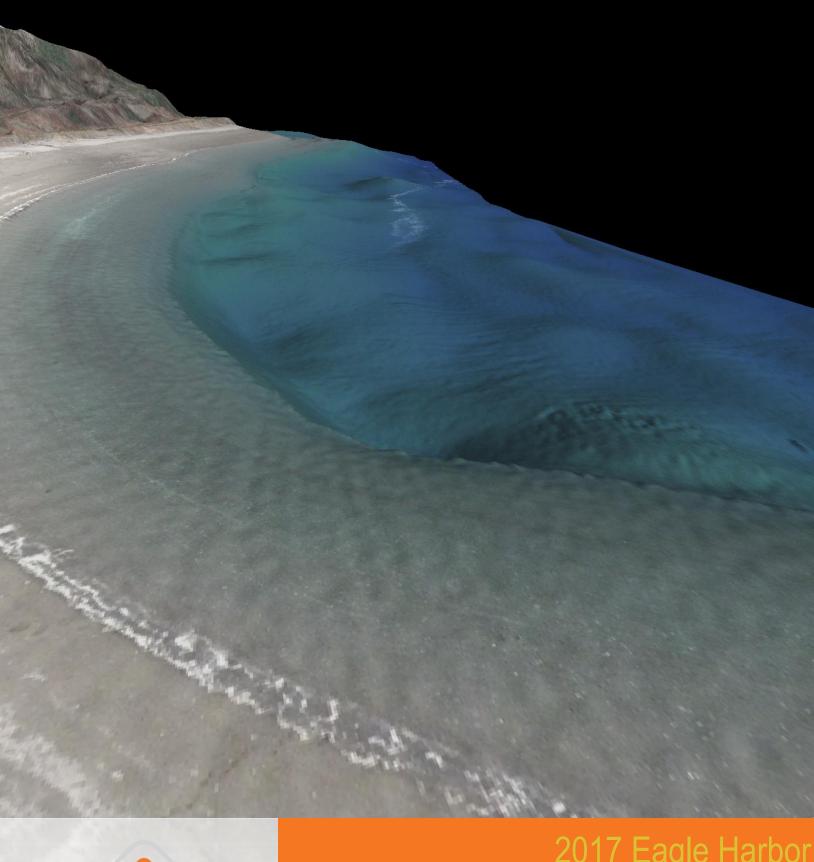
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Name (Print): // (Wildon)	Signature:
Name (Print): ANDRICAL SOMM	Signature: 4 .
Name (Print):	Signature:



### Appendix I-2a. MCA Orthophoto, Lidar, and Bathymetric Survey Report



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Orthophoto, Lidar and Bathymetric Survey Project Report

### **Contents**

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Summary	2
Lidar Acquisition	3
Survey Report	4
Data Processing	6
Quality Control	6
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### Summary

In summer 2017, Miller Creek Associates (MCA) teamed with APS Surveying and Mapping LLC (Ground Survey), Terrasond Ltd (Hydrographic) and Geoterra, Inc (Lidar) to provide mapping data for the Eagle Harbor site in Kitsap County, WA. The Lidar data was acquired with a planned nominal density of 8 points per square meter (PPSM) and was acquired during a -2.6' MLLW tide. Hydrographic data was acquired during a high tide to ensure sufficient overlap with the lidar data. Imagery was acquired during overcast conditions to ensure minimal shadows.

### **Lidar Details**

Acreage (Lidar/Orthophoto)	36
Flight Date	May 26 <sup>th</sup> , 2017
Coordinate System	Washington State Plane North
Horizontal Datum	NAD83(91)
Vertical Datum	MLLW (NAVD88 + 2.509')
Unit of Measure	US Survey Foot
Lidar Sensor	Optec Galaxy
Scan Rate	74 Hz
Pulse Rate	350 kHz
Final Point Density (Meters <sup>2</sup> )	12.29 pts/m²
Field of View (FOV)	30°
Altitude (Feet - AGL)	4900'
RMSEz (Feet)	0.083′

**Table 1 - Lidar Details** 

### **Orthophoto Details**

Acreage (Lidar/Orthophoto)	36
Flight Date	January 30, 2017
Coordinate System	Washington State Plane North
Horizontal Datum	NAD83(91)
Unit of Measure	US Survey Foot
Camera	Ultracam Falcon
Raw Pixel Resolution	.15 Foot
Orthophoto Pixel Resolution	.20 Foot
Final Orthophoto Specifications	8 Bit RGB / 8 Bit CIR
Overlap / Sidelap	60 / 45
Flight Altitude (Feet - AGL)	2000
Camera	Ultracam Falcon

**Table 2 - Orthophoto Details** 



Figure 1 – Ortho/Terrain view

### **Lidar Acquisition**

All lidar data was acquired on May 26th, 2017 during a single mission. The sensor used was an Optech Galaxy mounted in Cessna 310 fixed-wing aircraft. The flight plan was designed with a minimum of 50% overlap in swath footprint to minimize laser shadowing and data gaps. Flight planning was performed using Optech Flight Management System (FMS) software to calculate optimum parameters to meet project requirements and accommodate terrain variations. Airborne GPS and IMU data were acquired during flight to ensure a tight relative fit and georeference the data. Data was acquired at a -2.6' tide to ensure significant overlap between the lidar and hydrographic data.

### **Hydrographic Data Acquisition**

For details on the hydrographic mission, see 2017 EagleHarbor HydrographicSurvey Report.pdf

### **Image Acquisition**

Image acquisition of was performed on January 30, 2017 using a gyro-stabilized Ultracam Falcon digital image sensor mounted in a Cessna 206 StationAir. Imagery was acquired under highovercast conditions to minimize shadows. Image sidelap for the project was increased to 45% from the industry standard of 30%. This increased overlap serves to reduce the lean of trees and buildings and improves accuracy overall.

### **Survey Report**

After a tight relative fit was achieved, an absolute vertical offset was calculated using surveyed control points. MCA was provided with 57 ground control points. Of the 57 points, 40 of those were determined to be appropriate as vertical control points to be used to provide an absolute vertical offset for the final point cloud. Final RMSE on the points used for the vertical offset was .083'. Additionally, 9 ground control points were used in the aerotriagulation process to georeference the imagery.

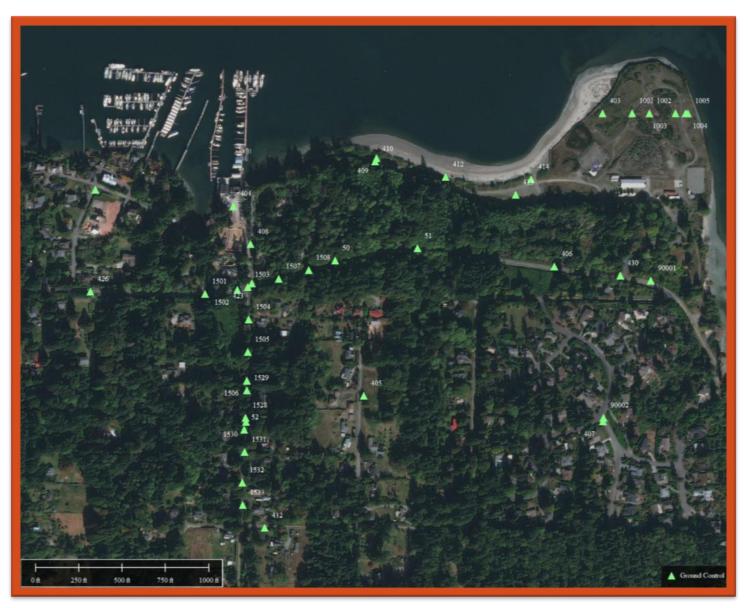


Figure 3 – Survey control distribution

### **Survey Control**

Point #	Х	v	-	Dz*
		Y 220264 425	Z 10.055	
410	1227556.551	229261.435	18.955	-0.151
1005	1229360.281	229537.828	18.049	-0.123
1001	1229039.518	229537.771	15.283	-0.115
413	1228367.065	229070.954	16.842	-0.113
1003	1229288.135	229537.757	15.168	-0.106
1532	1226790.120	227417.075	135.088	-0.104
1004	1229347.467	229537.682	15.749	-0.103
1533	1226792.721	227290.003	137.901	-0.102
50	1227327.281	228693.994	85.726	-0.096
1002	1229139.629	229537.807	13.877	-0.093
414	1228456.920	229160.290	17.910	-0.072
90001	1229148.016	228577.166	94.172	-0.051
1528	1226808.885	227789.366	114.407	-0.045
1530	1226812.749	227765.554	116.138	-0.035
52	1226801.238	227723.067	118.636	-0.025
408	1226839.121	228787.858	37.251	-0.023
1529	1226817.647	227947.138	100.195	-0.004
424	1225944.297	229099.173	44.505	0.001
403	1228868.774	229537.751	22.786	0.011
1504	1226826.600	228353.305	66.380	0.011
1508	1227174.487	228636.833	77.507	0.013
90002	1228873.734	227791.020	204.680	0.014
1503	1226823.843	228539.710	59.002	0.016
423	1226847.058	228561.782	58.462	0.017
430	1228970.743	228605.379	101.754	0.017
405	1227491.554	227916.866	191.850	0.017
406	1228592.213	228659.863	96.939	0.018
407	1228871.527	227769.831	205.819	0.024
1502	1226761.383	228524.860	58.727	0.032
1501	1226576.613	228502.178	65.988	0.035
1507	1227000.206	228587.509	67.818	0.038
51	1227801.480	228762.725	100.061	0.040
1506	1226818.687	228001.738	94.670	0.046
409	1227564.388	229280.907	18.974	0.095
432	1226919.195	227158.313	151.479	0.101
412	1227964.443	229173.690	17.391	0.117
1531	1226804.013	227593.020	125.120	0.125
404	1226739.411	229006.074	20.364	0.133
426	1225913.796	228513.325	98.453	0.163
1505	1226822.462	228168.323	76.936	0.184

Table 3 – Survey Control values

<sup>\*</sup> This value represents the difference between the value of the ground control and the value of the lidar.

### **Lidar Data Processing**

After primary data acquisition, the raw data is calibrated. This process includes relative adjustments between flight strips using common planes. Automatic point cloud classification was performed and significant water bodies were outlined for classification as water.

After initial point cloud calibration and geo-referencing, the TerraSolid software suite was used for automated point cloud classification. This process uses complex algorithms to analyze the point cloud and metadata, and classify ground, non-ground and anomalous high and low points. All tiles were edited manually to identify areas where the automated classification was insufficient, or where man-made structures require manual reclassification.

### **Lidar Quality Control**

MCA performed a comprehensive quality control assessment of the data. All datasets were checked against each other for consistency, accuracy and completeness. Specific quality control checks included the following:

- 1. Point cloud data checked against survey checkpoints for absolute accuracy
- 2. Inspection of all deliverables for completeness and accuracy
  - a. Map projection check
  - b. Data completeness check
  - c. Generation of shaded relief for visual QC

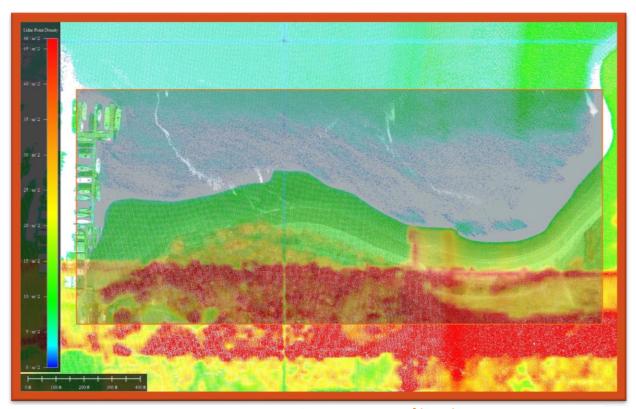


Figure 3 – First return point density in points per m<sup>2</sup> (PPSM)

### **Lidar Classifications**

Class	Description
1	Non-Ground
2	Ground
3	Low Vegetation
4	Medium Vegetation
5	High Vegetation
6	Building
7	Low Noise
9	Water

**Table 4 – Lidar Classifications** 

### **Deliverables**

### Lidar

All returns	LAS 1.2
Bare Earth	LAS 1.2
DEM (1ft)	ESRI
Lidar/Ortho Project Report	PFD

### Orthophoto

Natural Color RGB Orthophoto	TIFF/SID Mosaic
FCIR Orthophoto	TIFF/SID Mosaic
Tile Layout	Shape

### Hydrographic

ASCii Point	ТХТ
DEM (1ft and 3ft)	ESRI
Hill Shade Imagery	TIFF
Hydrographic Project Report	PFD

**Table 5 - Deliverables** 

### **Contact Info**



Miller Creek Associates Jeffrey Kenner, RPP, CP 19550 International Blvd STE 203 SeaTac, WA 98188 (206) 402-6052